

# *Solutions to Navigation Practice*

- 1a) Fl 6sec 64ft 15M HORN-- Flashing white light, 6 second period, 64 feet high, 15 mile light visibility with a horn.
- 1b) Gp Occ (1+2) 15sec 65ft 16M Racon-- Group occulting white light, 1 dark followed by 2 darks, 15 second period, 65 feet high with a radar responder.
- 1c) KGR- Rectangular green dayboard bearing a central red stripe.
- 1d) GR "A" Fl (2+1) G 6s-- Green over red channel junction buoy, group flashing green light, 1 flash followed by 2 flashes, 6 second period. For preferred channel, leave this buoy to port side when enter from sea.
  
- 2a) Drying heights and contours above chart datum; I-15 of Chart #1.
- 2b) Rock which covers and uncovers during tidal swings; number designates height in feet above chart datum when uncovered; refer to K11 of Chart #1.
- 2c) Dangerous wreck, depth unknown; refer to K28 of Chart #1.
- 2d. Oil or gas installation buoy, or catenary anchor leg mooring, or single buoy mooring; refer to L16 of Chart #1.
- 2e) Established (mandatory) direction of traffic flow; refer to M10 of Chart #1.
- 2f) Rip rap surrounding a light; refer to Pa of Chart #1.
- 2g) Mean lower low water; refer to H12 of Chart #1.
- 2h) Position doubtful; refer to B8 of Chart #1.
  
- 3a) Water depths
- 3b) Distances
- 3c) Bearings
  
- 4a) Description of the entire Nav Aid system in US waters.
- 4b) Locations of Nav Aids
- 4c) Light Characteristics and descriptions of specific Nav Aids
- 4d) Geographic range table
  
- 5a) USCG Light List for US waters
- 5b) NGA List of Lights for non-US waters
- 5c) Chart #1
- 5d) Ocean Pilot Charts
  
- 6) NOAA Website
  
- 7) Starboard
  
- 8a) USCG Notices to Mariners.
- 8b) NGA Website.
  
- 9a) Safe Water mark.

- 9b) Isolated Dangers mark.
- 9c) Unlighted green can; leave to portside entering from sea.
- 9d) Lighted yellow special mark.
- 9e) Black & white dayboard.

**Part II- Questions 10 to 15 contain 32 answers valued at 2 points each. Max points = 64.**

First, it is necessary to update the magnetic Variations on 1210Tr from the date of the chart. There are three compass roses on this chart and they all have a slightly different Variation, which range from 15°00'W in the SW corner of the chart to 15°30'W in the NE corner. All show an annual increase of 3'W, which needs to be applied for the elapsed 19 years from 1985 to 2004. Correct as follows:

$15^{\circ}00'W$ in 1985 $\underline{57'W}$ 19 x 3' $15^{\circ}57'W$ in 2004	$15^{\circ}30'W$ in 1985 $\underline{57'W}$ 19 x 3' $16^{\circ}27'W$ in 2004
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Round these off to a whole degree, which in both cases produce 16°W; therefore we can use 16°W Variation for the entire chart in the year 2004.

10) First plot your DR. Since the magnetic compass rose is out of date as discussed above, convert the course from °psc to °T using 16°W Variation as discussed above and the Deviation table earlier given:

	T	V	M	D	C
Course	231	16W	247	1E	246

Plot the DR from 0900 starting at buoy R"26" Fl R 4 sec Bell and draw in a course line at 231°T. Speed is given as 4.9 knots; spread your dividers to this distance using the latitude scale on the right or lefthand sides of the chart and mark the distance from 0900 to 1000, from 1000 to 1100 and from 1100 to 1130; mark these points with a half circle and a dot and write in the times. See attached plot 13-10a.

A three bearing fix was shot at 1130. One was a visual range based on the E end of Nashawena Island when it aligned perfectly with the W end of Pasque Island; draw in this line on the chart.

The other two bearings were shot across the ship's compass and need to be converted from °psc to °T as follows:

	T	V	M	D	C
Cuttyhunk	301	16W	317	1E	316
Gay Head	138	16W	154	1E	153

Plot these two additional bearings and you'll find that they cross very close to a single point as shown in the attached plot; this is your 1130 Fix; mark it with a circle and a dot and write in the time of 1130. See attached plot 13-10b.

The 1130 Fix is not at the 1130 DR position. The difference is attributed to current assumed to be acting on the boat over the previous 2-1/2 hours. You were pushed from the DR to the Fix by the current. Draw in this line and measure its direction by transferring it with parallel rules to the compass rose; it should be 280°T, which is assumed to be the current Set.

Measure the distance from the DR to the Fix and it should be 0.64 NM; this is not the current Drift velocity, it's the distance that the current pushed us during a 2-1/2 hour period. So, Drift velocity is:

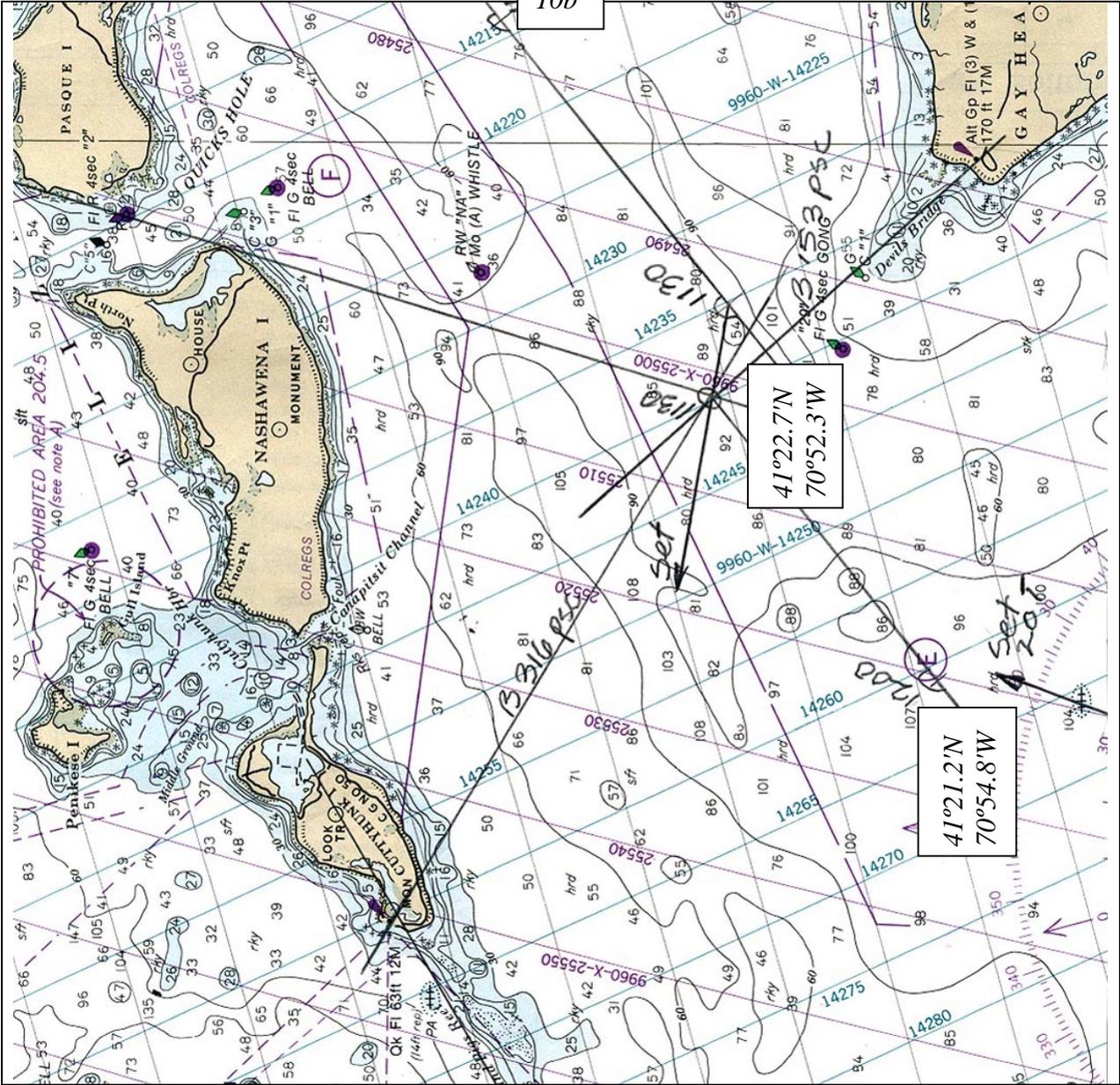
$$\text{Drift} = 0.64 \text{ NM} \div 2.5 \text{ hours} = 0.26 \text{ knots}$$

From the Fix continue plotting the DR from 1130 to 1200 and mark this point with a half circle and a dot.

Determine the latitudes and longitudes of the 1130 DR, the 1130 fix and the 1200 DR.



10b

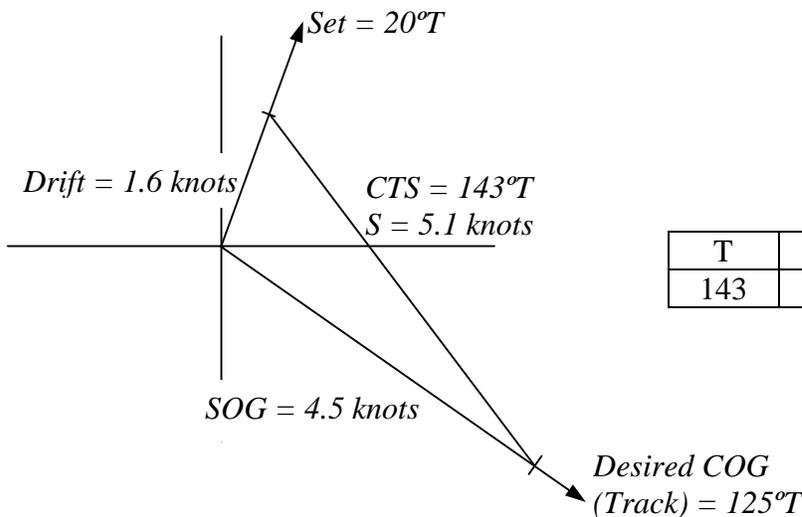


11) Plot the desired COG (Track) from buoy BW "VS" Whistle to buoy R"2" Fl R 4 sec Whistle; it should be  $125^{\circ}T$ . You need to determine the course to steer needed to compensate for the current flow and stay on your desired course. This is a Type C current problem as discussed in Chapter 7 of the text; here's what you know:

C	?
S	5.1 knots
Set	$20^{\circ}T$
Drift	1.6 knots
COG	$125^{\circ}T$
SOG	?

Plot the COG of  $125^{\circ}T$ . Plot the Set of  $20^{\circ}T$ . Measure the Drift velocity of 1.6 knots along the Set vector and place a mark there.

Now, adjust your dividers to the boat speed S of 5.1 knots; place one end of the dividers at the end of the current vector and swing the other end of the dividers to find where it touches the COG vector; put a mark at this point.



T	V	M	D	C
143	16W	159	2W	161

Speed over ground is determined by measuring the length on the "over ground" side of the triangle, which should be 4.5 knots. Use this speed to determine the ETA at buoy R"2" Fl R 4 sec Whistle as follows:

$$\begin{aligned}
 \text{Transit time} &= \text{Distance} \div \text{SOG} \\
 &= 9.3 \text{ NM} \div 4.5 \text{ knots} \\
 &= 2.066 \text{ hours} \\
 &= 2 \text{ hours \& 04 minutes.}
 \end{aligned}$$

$$\begin{aligned}
 \text{ETA} &= \text{Departure time} + \text{Transit Time} \\
 &= 1300 + 0204 \\
 &= 1504
 \end{aligned}$$

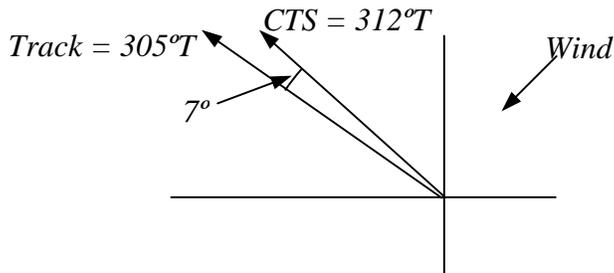


12) The desired COG (Track) for this question is the reciprocal of that for question #11, or

$$\text{Track} = 125^\circ\text{T} + 180^\circ = 305^\circ\text{T}$$

	T	V	M	D	C
Track	305	16W	321	1W	322

To counteract the NE wind and stay on track you need to steer toward the wind by the amount of the leeway or  $7^\circ$ , thus:



	T	V	M	D	C
CTS	312	16W	328	1W	329

13-13) Draw a danger bearing line from the G "5" Fl G 4 sec Gong buoy to the BW "BB" Mo(A) Bell buoy and notice that the wreck lies just N of this line. This bearing line is  $71^\circ\text{T}$ , which we need to convert to psc to allow monitoring on the ship's compass.

	T	V	M	D	C
Bearing	71	16W	87	4W	91

We want to stay S of this line to remain away from the wreck. This danger bearing line is NOT a course line; we may choose to sail on a course below it and remain further away from the wreck. While doing this, we monitor the compass bearing to the BW "BB" Mo(A) Bell buoy; as long as this bearing remains LESS than  $91^\circ\text{psc}$ ; we'll be away from the wreck.

Bearings of more than  $91^\circ\text{psc}$  would put us N of the danger bearing line.



14) This is a running fix question. First draw in the desired COG (Track) from the BW "BB" Mo(A) Bell buoy to the Fl 10 sec 74ft 16M HORN R Bn 308 beacon at Cleveland Ledge Channel; it should be 42°T; convert to °psc as follows:

	T	V	M	D	C
Track	42	16W	58	4W	62

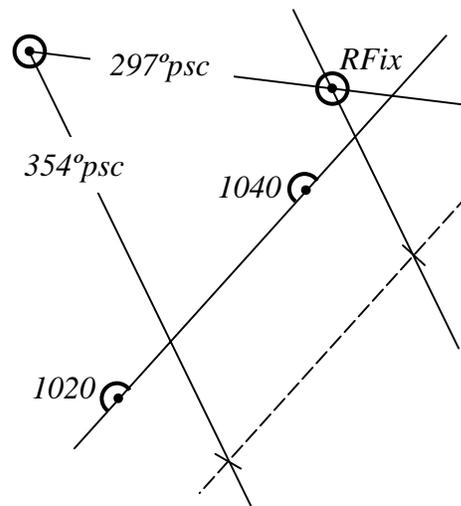
Initially, you'll steer the 62°psc lacking any information about current or leeway.

Since bearings were shot on the tower at 1020 and 1040, you'll need to locate your DR positions for these times. Calculate the distance traveled from 1000 to 1020 at a boat speed of 6.2 knots. This is 1/3 hour, so distance is 1/3 hour x 6.2 knots = 2.1 NM. Measure this distance and mark the point with a dot and half circle on the course line. Do the same for 1040.

Convert these bearings from °psc to °T as follows and draw them in on the chart.

	T	V	M	D	C
1020 Bearing	334	16W	350	4W	354
1040 Bearing	277	16W	293	4W	297

Advance the 1020 bearing line in the direction and distance of the DR between 1020 and 1040. This is done by drawing a line parallel to the course line between 1020 and 1040 and marking off the distance covered by the DR in that time starting from where this line intersects the 1020 bearing line.



As shown in the next plot, the actual COG achieved is 35°T from the starting buoy to the RFix, and the wind leeway is therefore 42°T - 35°T = 7° to port.

The desired course (Track) from the RFix to the destination buoy is 48°T and you'll need to steer toward the wind (to the right) by 7° in order to stay on track. So, CTS = 48°T + 7° = 55°T and this converts to 75°psc.



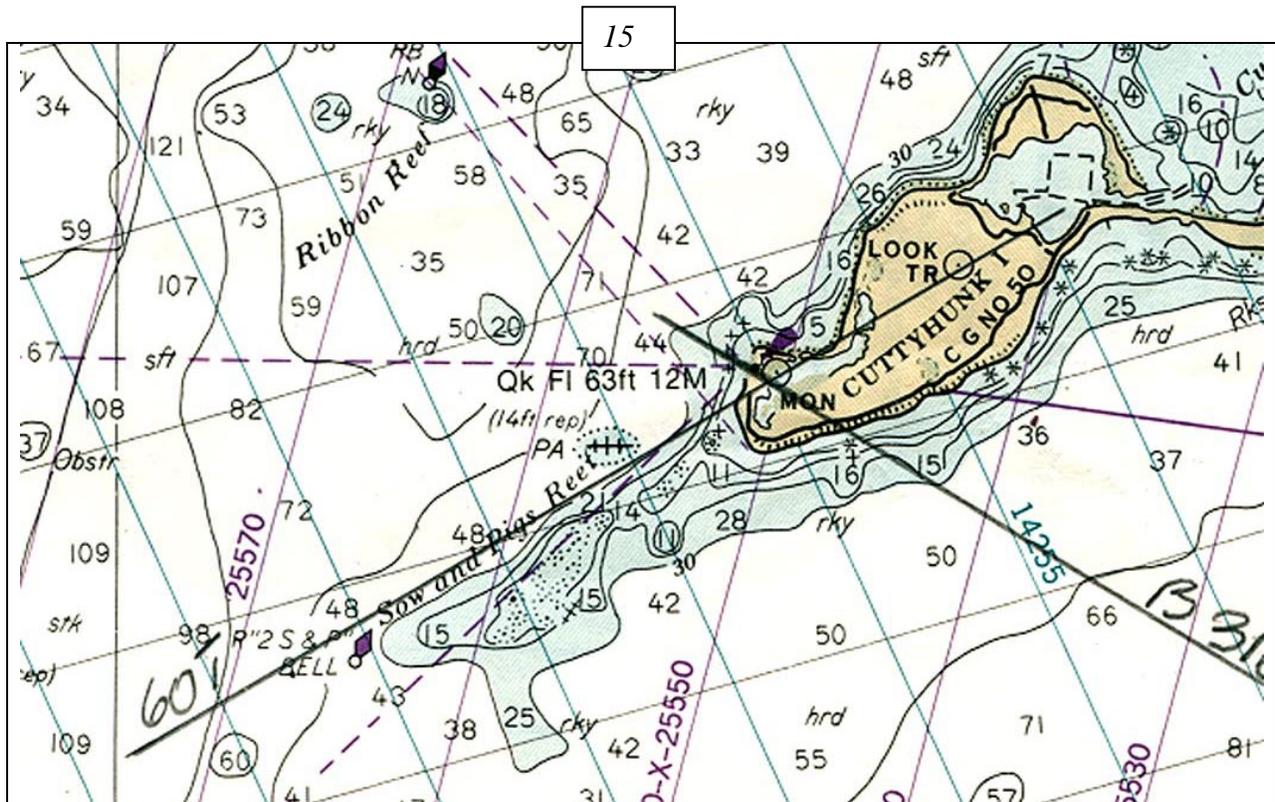
15) This question verifies the accuracy of the Deviation table while on one boat heading of 344°psc. Using a pelorus you shot the range between the two towers on Cuttyhunk and found it to be 98° relative off of your starboard bow. Therefore, the bearing along the range between the towers, based on the compass is:

$$\begin{aligned} \text{Bearing of range} &= 344^\circ\text{psc} + 98^\circ \\ &= 442^\circ\text{psc} - 360^\circ \\ &= 82^\circ\text{psc} \end{aligned}$$

The chart shows this range to be 60°T, and we enter this information in the table as follows:

	T	V	M	D	C
Range	60	16W	76	6W	82

From this observation we compute the compass deviation to be 6°W for a boat heading of 344°psc, but the Deviation table gives 1°W for this heading. So, either the Deviation table is in error or our shot was in error.



16) What is the time and height of the lowest tide at Newport, RI on January 29, 1997? This is a direct lookup in the tide table of Appendix G-15.

## Newport, R.I., 1997

### Times and Heights of High and Low Waters

January				February				March																					
Time	Height			Time	Height			Time	Height			Time	Height																
	h	m	ft	cm		h	m	ft	cm		h	m	ft	cm		h	m	ft	cm										
<b>1</b> W	0037	2.9	88		<b>16</b> Th	0126	3.7	113		<b>1</b> Sa	0142	3.1	94		<b>16</b> Su	0258	3.4	104		<b>1</b> Sa	0007	3.2	98		<b>16</b> Su	0125	3.3	101	
	0537	0.5	15			0733	0.2	6			0656	0.4	12			0955	0.5	15			0527	0.2	6			0741	0.6	18	
	1255	2.8	85			1352	3.2	98			1407	2.7	82			1525	2.9	88			1234	2.8	85			1355	2.8	85	
	1802	0.3	9			1943	0.1	3			1913	0.1	3			2145	0.4	12			1742	0.1	3			1938	0.6	18	
<b>2</b> Th	0130	3.0	91		<b>17</b> F	0227	3.7	113		<b>2</b> Su	0242	3.3	101		<b>17</b> M	0356	3.4	104		<b>2</b> Su	0106	3.2	98		<b>17</b> M	0226	3.2	98	
	0634	0.6	18			0859	0.3	9			0806	0.3	9			1055	0.4	12			0626	0.3	9			0917	0.6	18	
	1350	2.8	85			1453	3.1	94			1508	2.8	85			1620	3.0	91			1336	2.8	85			1455	2.8	85	
	1855	0.3	9			2055	0.2	6			2020	0.0	0			2247	0.3	9			1843	0.1	3			2118	0.6	18	
<b>3</b> F	0225	3.1	94		<b>18</b> Sa	0326	3.7	113		<b>3</b> M	0341	3.6	110		<b>18</b> Tu	0448	3.5	107		<b>3</b> M	0210	3.3	101		<b>18</b> Tu	0325	3.1	94	
	0738	0.6	18			1015	0.3	9			0918	0.1	3			1139	0.3	9			0735	0.2	6			1022	0.6	18	
	1446	2.8	85			1550	3.1	94			1607	3.1	94			1709	3.1	94			1441	2.9	88			1551	2.9	88	
	1954	0.2	6			2203	0.1	3			2128	-0.2	-6			2331	0.2	6			1953	0.1	3			2227	0.5	15	
<b>4</b> Sa	0320	3.3	101		<b>19</b> Su	0421	3.7	113		<b>4</b> Tu	0437	3.9	119		<b>19</b> W	0535	3.6	110		<b>4</b> Tu	0313	3.5	107		<b>19</b> W	0418	3.2	98	
	0846	0.4	12			1112	0.2	6			1025	-0.1	-3			1212	0.2	6			0850	0.1	3			1104	0.5	15	
	1542	2.9	88			1644	3.1	94			1703	3.4	104			1755	3.3	101			1543	3.2	98			1641	3.1	94	
	2056	0.1	3			2257	0.1	3			2234	-0.4	-12								2109	-0.1	-3			2311	0.4	12	
<b>5</b> Su	0412	3.6	110		<b>20</b> M	0512	3.8	116		<b>5</b> W	0531	4.2	128		<b>20</b> Th	0006	0.0	0		<b>5</b> W	0413	3.8	116		<b>20</b> Th	0506	3.3	101	
	0951	0.2	6			1158	0.1	3			1125	-0.5	-15			0618	3.7	113			1002	-0.2	-6			1134	0.3	9	
	1635	3.2	98			1733	3.2	98			1756	3.8	116			1238	0.1	3			1641	3.6	110			1727	3.3	101	
	2157	-0.2	-6			2342	0.0	0			2335	-0.7	-21			1837	3.5	107			2220	-0.4	-12			2344	0.2	6	
<b>6</b> M	0503	4.0	122		<b>21</b> Tu	0558	3.9	119		<b>6</b> Th	0622	4.5	137		<b>21</b> F	0036	-0.1	-3		<b>6</b> Th	0509	4.1	125		<b>21</b> F	0549	3.5	107	
	1051	-0.1	-3			1234	0.0	0			1218	-0.8	-24			0659	3.7	113			1104	-0.5	-15			1159	0.2	6	
	1727	3.4	104			1818	3.3	101			1847	4.1	125			1301	0.0	0			1735	4.0	122			1809	3.6	110	
	2254	-0.4	-12												1917	3.6	110			2324	-0.7	-21							
<b>7</b> Tu	0553	4.3	131		<b>22</b> W	0019	-0.1	-3		<b>7</b> F	0031	-1.0	-30		<b>22</b> Sa	0105	-0.2	-6		<b>7</b> F	0602	4.4	134		<b>22</b> Sa	0013	0.0	0	
	1146	-0.4	-12			0642	3.9	119			0713	4.7	143			0738	3.8	116			1158	-0.8	-24			0631	3.6	110	
	1817	3.7	113			1303	0.0	0			1309	-1.0	-30			1326	-0.1	-3			1827	4.3	131			1223	0.0	0	
	2349	-0.7	-21			1901	3.4	104			1937	4.4	134			1956	3.6	110								1849	3.7	113	
<b>8</b> W	0642	4.6	140		<b>23</b> Th	0052	-0.1	-3		<b>8</b> Sa	0124	-1.1	-34		<b>23</b> Su	0135	-0.2	-6		<b>8</b> Sa	0020	-1.0	-30		<b>23</b> Su	0042	-0.1	-3	
	1237	-0.7	-21			0723	3.9	119			0803	4.7	143			0817	3.7	113			0653	4.6	140			0710	3.7	113	
	1907	3.9	119			1329	-0.1	-3			1357	-1.1	-34			1353	-0.2	-6			1248	-1.0	-30			1250	-0.1	-3	
						1942	3.5	107			2027	4.5	137			2035	3.6	110			1917	4.6	140			1928	3.8	116	
<b>9</b> Th	0042	-0.9	-27		<b>24</b> F	0124	-0.2	-6		<b>9</b> Su	0216	-1.1	-34		<b>24</b> M	0207	-0.2	-6		<b>9</b> Su	0113	-1.1	-34		<b>24</b> M	0112	-0.2	-6	
	0731	4.7	143			0803	3.9	119			0852	4.6	140			0855	3.6	110			0743	4.6	140			0749	3.7	113	
	1326	-0.9	-27			1355	-0.1	-3			1444	-1.0	-30			1422	-0.2	-6			1335	-1.1	-34			1320	-0.2	-6	
	1956	4.1	125			2023	3.5	107			2117	4.5	137			2113	3.6	110			2006	4.7	143			2006	3.9	119	
<b>10</b> F	0134	-1.0	-30		<b>25</b> Sa	0155	-0.2	-6		<b>10</b> M	0307	-1.0	-30		<b>25</b> Tu	0240	-0.2	-6		<b>10</b> M	0203	-1.2	-37		<b>25</b> Tu	0144	-0.3	-9	
	0821	4.7	143			0843	3.8	116			0943	4.4	134			0932	3.4	104			0832	4.5	137			0827	3.6	110	
	1414	-0.9	-27			1422	-0.1	-3			1531	-0.9	-27			1453	-0.2	-6			1421	-1.0	-30			1351	-0.2	-6	
	2047	4.2	128			2103	3.4	104			2209	4.4	134			2152	3.5	107			2055	4.7	143			2044	3.9	119	
<b>11</b> Sa	0226	-1.0	-30		<b>26</b> Su	0228	-0.1	-3		<b>11</b> Tu	0359	-0.7	-21		<b>26</b> W	0315	-0.1	-3		<b>11</b> Tu	0252	-1.0	-30		<b>26</b> W	0218	-0.3	-9	
	0911	4.6	140			0922	3.6	110			1034	4.1	125			1011	3.2	98			0921	4.3	131			0906	3.5	107	
	1503	-0.9	-27			1452	-0.1	-3			1618	-0.6	-18			1528	-0.1	-3			1506	-0.8	-24			1424	-0.2	-6	
	2138	4.2	128			2143	3.4	104			2302	4.1	125			2232	3.4	104			2144	4.5	137			2123	3.8	116	
<b>12</b> Su	0319	-0.8	-24		<b>27</b> M	0302	0.0	0		<b>12</b> W	0452	-0.4	-12		<b>27</b> Th	0353	0.0	0		<b>12</b> W	0341	-0.7	-21		<b>27</b> Th	0254	-0.3	-9	
	1003	4.4	134			1001	3.4	104			1128	3.7	113			1052	3.0	91			1011	4.0	122			0946	3.3	101	
	1552	-0.8	-24			1524	-0.1	-3			1708	-0.3	-9			1606	-0.1	-3			1551	-0.6	-18			1501	-0.2	-6	
	2232	4.1	125			2224	3.2	98			2358	3.9	119			2316	3.3	101			2235	4.2	128			2203	3.7	113	
<b>13</b> M	0413	-0.6	-18		<b>28</b> Tu	0338	0.1	3		<b>13</b> Th	0551	-0.1	-3		<b>28</b> F	0437	0.1	3		<b>13</b> Th	0430	-0.4	-12		<b>28</b> 				

17) What is the time and height of the lowest tide at Portland Head Light on February 18, 1997?

From Appendix page G-12 find Portland Head Light #869 and a Low Water height ratio of 0.97 and a time difference of -2 minutes compared with the reference station at Portland, Maine.

Portland, Maine on Appendix page G-14 for February 18, 1997 gives the lowest tide height as 0.3 feet at 1448.

Therefore, at Portland Head Light, Low Water would be:

$$\text{Time} = 1448 - 0002 = 1446 \text{ hours/minutes}$$

$$\text{Height} = 0.3 \text{ feet} \times 0.97 = 0.29 \text{ feet}$$

18) Convert Eastern Standard Time to Eastern Daylight Time.

$$\text{EDT} = \text{EST} + 1 \text{ hour}$$

19) What is the time of the maximum flood current at Boston Harbor, Deer Island Light on February 19, 1997? This is a straight lookup on *Appendix page I-8*.

13-20) What is the direction, velocity and time of the maximum ebb current at Wareham River off Barney's Point on January 23, 1997?

On *Appendix page I-7* find Wareham River, Barney's Point # 2141

- Time difference is given as - 1 hour & 31 minutes under Ebb
- Speed Ratio is given as 0.4 under Ebb.
- In the right hand column under Max Ebb the direction is given as 185°T.
- Reference Station is given as Pollock Rip Channel

On *Appendix page I-9* find Pollock Rip Channel daily predictions

- Max Ebb current is given at 1.8 knots at 1212
- At Wareham River, Barney's Point:

$$\text{Time} = 1212 - 0131 = 1041 \text{ EST}$$

$$\text{Velocity} = 1.8 \text{ knots} \times 0.4 = 0.72 \text{ knots}$$

TABLE 2 – TIDAL DIFFERENCES AND OTHER CONSTANTS

No.	PLACE	POSITION		DIFFERENCES				RANGES		Mean Tide Level
		Latitude	Longitude	Time		Height		Mean	Spring	
				High Water	Low Water	High Water	Low Water			
	MAINE, Casco Bay--cont. Time meridian, 75° W	North	West	h m	h m	ft	ft	ft	ft	
				on Portland, p.32						
833	Little Flying Point, Maquoit Bay	43° 50'	70° 03'	-0 01	-0 01	*0.99	*0.99	9.0	10.3	4.8
835	South Freeport	43° 49'	70° 06'	+0 12	+0 10	*0.99	*0.99	9.0	10.3	4.8
837	Chebeague Point, Great Chebeague Island	43° 46'	70° 06'	-0 04	-0 09	*0.99	*0.99	9.0	10.4	4.8
839	Prince Point	43° 46'	70° 10'	0 00	0 00	*1.01	*1.00	9.2	10.6	4.9
841	Doyle Point	43° 45'	70° 08'	-0 02	-0 03	*1.00	*0.88	9.2	10.5	4.9
843	Falmouth Foreside	43° 44'	70° 12'	+0 01	0 00	*1.00	*1.03	9.1	10.5	4.9
845	Great Chebeague Island	43° 43'	70° 08'	+0 03	+0 03	*1.00	*1.00	9.1	10.5	4.9
847	Cliff Island, Luckse Sound	43° 42'	70° 07'	-0 02	-0 02	*1.00	*1.00	9.1	10.4	4.9
849	Vaill Island	43° 41'	70° 09'	+0 05	+0 01	*0.98	*1.03	9.0	10.3	4.8
851	Long Island	43° 41'	70° 10'	-0 01	0 00	*1.00	*1.00	9.1	10.4	4.9
853	Cow Island	43° 41'	70° 11'	-0 01	0 00	*1.00	*1.00	9.1	10.5	4.9
855	Presumpscot River Bridge	43° 41'	70° 15'	+0 01	+0 04	*1.01	*1.06	9.2	10.6	5.0
857	Back Cove	43° 41'	70° 15'	+0 02	+0 06	*0.97	*0.97	9.1	10.5	4.9
859	Great Diamond Island	43° 40'	70° 12'	-0 01	0 00	*0.99	*1.00	9.0	10.4	4.9
861	Peaks Island	43° 39'	70° 12'	-0 04	-0 08	*0.99	*0.99	9.0	10.4	4.8
863	Cushing Island	43° 39'	70° 12'	+0 01	0 00	*0.99	*1.00	9.0	10.4	4.9
865	PORTLAND	43° 40'	70° 15'	Daily predictions				9.1	10.4	4.9
867	Fore River	43° 38'	70° 17'	+0 02	+0 02	*1.00	*1.06	9.1	10.5	4.9
869	Portland Head Light	43° 37'	70° 12'	-0 02	-0 02	*0.97	*0.97	8.9	10.2	4.8
	MAINE, outer coast--cont.									
871	Richmond Island	43° 33'	70° 14'	-0 03	-0 03	*0.98	*0.98	8.9	10.1	4.8
873	Old Orchard Beach	43° 31'	70° 22'	0 00	-0 06	*0.97	*0.97	8.8	10.1	4.7
875	Wood Island Harbor	43° 27'	70° 21'	+0 02	-0 04	*0.96	*0.96	8.7	9.9	4.7
877	Cape Porpoise	43° 22'	70° 26'	+0 12	+0 14	*0.95	*0.95	8.7	9.9	4.7
879	Kennebunkport	43° 21'	70° 28'	+0 16	+0 16	*0.94	*0.94	8.6	9.9	4.6
881	York Harbor	43° 08'	70° 38'	+0 03	+0 13	*0.95	*0.95	8.6	9.9	4.6
883	Seapoint, Cutts Island	43° 05'	70° 40'	+0 01	-0 04	*0.96	*0.96	8.8	10.1	4.7
	MAINE and NEW HAMPSHIRE									
	Portsmouth Harbor									
885	Jaffrey Point	43° 03'	70° 43'	-0 03	-0 05	*0.95	*0.95	8.7	10.0	4.7
887	Gerrish Island	43° 04'	70° 42'	-0 02	-0 03	*0.95	*0.95	8.7	10.0	4.7
889	Fort Point	43° 04'	70° 43'	+0 03	+0 07	*0.94	*0.94	8.6	9.9	4.6
891	Kittery Point	43° 05'	70° 42'	-0 07	+0 01	*0.96	*0.96	8.7	10.0	4.7
893	Seavey Island	43° 05'	70° 45'	+0 20	+0 18	*0.89	*0.89	8.1	9.4	4.4
895	Portsmouth	43° 05'	70° 45'	+0 22	+0 17	*0.86	*0.86	7.8	9.0	4.2
	Piscataqua River									
897	Atlantic Heights	43° 05'	70° 46'	+0 37	+0 28	*0.82	*0.82	7.5	8.6	4.0
899	Dover Point	43° 07'	70° 50'	+1 33	+1 27	*0.70	*0.70	6.4	7.4	3.4
901	Salmon Falls River entrance	43° 11'	70° 50'	+1 35	+1 52	*0.75	*0.75	6.8	7.8	3.6
903	Squamscott River RR. Bridge	43° 03'	70° 55'	+2 19	+2 41	*0.75	*0.75	6.8	7.8	3.6
905	Gosport Harbor, Isles of Shoals	42° 59'	70° 37'	+0 02	-0 02	*0.93	*0.93	8.5	9.8	4.5
907	Hampton Harbor	42° 54'	70° 49'	+0 14	+0 32	*0.91	*0.91	8.3	9.5	4.5
	MASSACHUSETTS, outer coast									
909	Merrimack River entrance	42° 49'	70° 49'	+0 20	+0 24	*0.91	*0.91	8.3	9.5	4.4
911	Newburyport, Merrimack River	42° 49'	70° 52'	+0 31	+1 11	*0.86	*0.86	7.8	9.0	4.2
913	Plum Island Sound (south end)	42° 43'	70° 47'	+0 12	+0 37	*0.94	*0.94	8.6	9.9	4.6
915	Annisquam	42° 39'	70° 41'	0 00	-0 07	*0.96	*0.96	8.7	10.1	4.7
917	Rockport	42° 40'	70° 37'	+0 04	+0 02	*0.94	*0.94	8.6	10.0	4.6
	on Boston, p.36									
919	Gloucester Harbor	42° 36'	70° 40'	-0 01	-0 04	*0.91	*0.91	8.7	10.1	4.6
921	Manchester Harbor	42° 34'	70° 47'	0 00	-0 04	*0.92	*0.92	8.8	10.2	4.7
923	Beverly	42° 32'	70° 53'	+0 02	-0 03	*0.94	*0.94	9.0	10.4	4.8
925	Salem	42° 31'	70° 53'	+0 04	+0 03	*0.92	*0.92	8.8	10.2	4.7
927	Marblehead	42° 30'	70° 51'	0 00	-0 04	*0.95	*0.95	9.1	10.6	4.8
	Broad Sound									
929	Nahant	42° 25'	70° 55'	+0 01	0 00	*0.94	*0.94	9.0	10.4	4.8
931	Lynn Harbor	42° 27'	70° 58'	+0 10	+0 06	*0.96	*0.96	9.2	10.7	4.9
	Boston Harbor									
933	Boston Light	42° 20'	70° 53'	+0 02	+0 03	*0.94	*0.94	9.0	10.4	4.8
935	Lovell Island, The Narrows	42° 20'	70° 56'	+0 04	+0 03	*0.95	*0.95	9.1	10.6	4.8
937	Deer Island (south end)	42° 21'	70° 58'	+0 01	0 00	*0.97	*0.97	9.3	10.8	4.9
939	Belle Isle Inlet entrance	42° 23'	71° 00'	+0 20	+0 17	*1.00	*1.00	9.5	11.0	5.0
941	Castle Island	42° 20'	71° 01'	0 00	+0 02	*0.99	*0.99	9.4	10.9	5.0
943	BOSTON	42° 21'	71° 03'	Daily predictions				9.5	11.0	5.1
945	Dover St. Bridge, Fort Point Channel	42° 21'	71° 04'	+0 06	+0 08	*1.01	*1.01	9.6	11.0	5.1
	Charles River									
947	Charlestown Bridge	42° 22'	71° 04'	+0 04	+0 04	*1.00	*1.00	9.5	11.0	5.0
949	Charles River Dam	42° 22'	71° 04'	+0 07	+0 06	*1.00	*1.00	9.5	11.0	5.0
951	Charlestown	42° 22'	71° 03'	0 00	+0 01	*1.00	*1.00	9.5	11.0	5.0
953	Chelsea St. Bridge, Chelsea River	42° 23'	71° 01'	+0 01	+0 06	*1.01	*1.01	9.6	11.1	5.1
955	Neponset, Neponset River	42° 17'	71° 02'	-0 02	+0 03	*1.00	*1.00	9.5	11.0	5.0
957	Moon Head	42° 19'	70° 59'	+0 01	+0 04	*0.99	*0.99	9.4	10.9	5.0
959	Rainsford Island, Nantasket Roads	42° 19'	70° 57'	0 00	+0 02	*0.95	*0.95	9.1	10.6	4.8

Endnotes can be found at the end of table 2.

## Portland, Maine, 1997

### Times and Heights of High and Low Waters

January				February				March												
Time	Height																			
	h	m	ft	h	m	ft	cm	h	m	ft	cm	h	m	ft	cm					
<b>1</b> W	0349	8.4	256	<b>16</b> Th	0449	9.9	302	<b>1</b> Sa	0438	8.9	271	<b>16</b> Su	0308	9.2	280	<b>16</b> Su	0449	9.3	283	
	0954	1.5	46		1107	0.0	0		1058	1.0	30		0927	0.6	18		1117	0.5	15	
	1604	8.3	253		1721	9.1	277		1709	8.1	247		1540	8.4	256		1734	8.3	253	
	2215	1.1	34		2328	0.1	3		2313	1.1	34		2143	0.9	27		2335	1.3	40	
<b>2</b> Th	0437	8.5	259	<b>17</b> F	0552	9.8	299	<b>2</b> Su	0533	9.0	274	<b>17</b> M	0109	1.1	34	<b>2</b> Su	0359	9.2	280	
	1048	1.4	43		1215	0.1	3		1158	0.7	21		1022	0.6	18		1022	0.6	18	
	1657	8.1	247		1828	8.8	268		1811	8.1	247		1636	8.3	253		1636	8.3	253	
	2305	1.2	37										2239	1.0	30		2239	1.0	30	
<b>3</b> F	0527	8.7	265	<b>18</b> Sa	0032	0.5	15	<b>3</b> M	0012	0.9	27	<b>18</b> Tu	0207	1.0	30	<b>3</b> M	0457	9.3	283	
	1144	1.3	40		0655	9.7	296		0632	9.4	287		0824	0.3	283		1125	0.5	15	
	1754	8.0	244		1319	0.1	3		1300	0.3	9		1448	0.3	9		1740	8.3	253	
	2358	1.1	34		1933	8.6	262		1914	8.4	256		2101	8.5	259		2342	0.9	27	
<b>4</b> Sa	0619	8.9	271	<b>19</b> Su	0132	0.6	18	<b>4</b> Tu	0113	0.6	18	<b>19</b> W	0258	0.9	27	<b>4</b> Tu	0601	9.5	290	
	1241	0.9	27		0753	9.7	296		0732	9.9	302		0913	9.4	287		1230	0.2	6	
	1851	8.2	250		1418	0.0	0		1401	-0.2	-6		1535	0.2	6		1847	8.5	259	
					2031	8.6	262		2014	8.8	268		2146	8.6	262		2030	8.4	256	
<b>5</b> Su	0052	1.0	30	<b>20</b> M	0228	0.6	18	<b>5</b> W	0212	0.2	6	<b>20</b> Th	0342	0.7	21	<b>5</b> W	0048	0.6	18	
	0712	9.4	287		0846	9.8	299		0830	10.5	320		0956	9.6	293		0707	9.9	302	
	1337	0.4	12		1511	-0.1	-3		1457	-0.9	-27		1615	0.1	3		1335	-0.2	-6	
	1948	8.4	256		2123	8.7	265		2111	9.4	287		2226	8.8	268		1951	9.1	277	
<b>6</b> M	0145	0.7	21	<b>21</b> Tu	0318	0.6	18	<b>6</b> Th	0309	-0.4	-12	<b>21</b> F	0422	0.6	18	<b>6</b> Th	0152	0.1	3	
	0804	9.9	302		0934	9.9	302		0926	11.0	335		1035	9.6	293		0810	10.4	317	
	1430	-0.2	-6		1557	-0.2	-6		1550	-1.5	-46		1651	0.0	0		1435	-0.8	-24	
	2042	8.8	268		2209	8.8	268		2204	10.0	305		2302	9.0	274		2050	9.7	296	
<b>7</b> Tu	0238	0.3	9	<b>22</b> W	0402	0.6	18	<b>7</b> F	0403	-0.9	-27	<b>22</b> Sa	0458	0.4	12	<b>7</b> F	0252	-0.5	-15	
	0855	10.5	320		1016	9.9	302		1020	11.5	351		1110	9.7	296		0909	10.9	332	
	1521	-0.8	-24		1639	-0.3	-9		1641	-1.9	-58		1724	0.0	0		1530	-1.3	-40	
	2134	9.3	283		2250	8.8	268		2256	10.5	320		2334	9.1	277		2144	10.4	317	
<b>8</b> W	0329	-0.2	-6	<b>23</b> Th	0442	0.5	15	<b>8</b> Sa	0457	-1.4	-43	<b>23</b> Su	0533	0.3	9	<b>8</b> Sa	0349	-1.2	-37	
	0945	11.0	335		1055	9.9	302		1112	11.7	357		1144	9.6	293		1005	11.3	344	
	1611	-1.3	-40		1716	-0.3	-9		1732	-2.1	-64		1755	0.0	0		1622	-1.7	-52	
	2224	9.7	296		2327	8.9	271		2347	10.8	329						2236	10.9	332	
<b>9</b> Th	0420	-0.6	-18	<b>24</b> F	0520	0.5	15	<b>9</b> Su	0550	-1.6	-49	<b>24</b> M	0006	9.1	277	<b>9</b> Su	0443	-1.6	-49	
	1035	11.4	347		1131	9.8	299		1205	11.6	354		0606	0.3	9		1058	11.5	351	
	1700	-1.7	-52		1751	-0.2	-6		1822	-2.1	-64		1217	9.5	290		1712	-1.9	-58	
	2314	10.1	308									1826	0.1	3		2326	11.3	344		
<b>10</b> F	0512	-0.9	-27	<b>25</b> Sa	0002	8.9	271	<b>10</b> M	0038	11.0	335	<b>25</b> Tu	0037	9.2	280	<b>10</b> M	0535	-1.9	-58	
	1127	11.6	354		0555	0.6	18		0644	-1.6	-49		0640	0.3	9		1150	11.5	351	
	1750	-2.0	-61		1206	9.7	296		1259	11.3	344		1251	9.3	283		1801	-1.8	-55	
					1824	-0.1	-3		1913	-1.8	-55		1858	0.2	6					
<b>11</b> Sa	0005	10.3	314	<b>26</b> Su	0036	8.9	271	<b>11</b> Tu	0130	10.9	332	<b>26</b> W	0109	9.2	280	<b>11</b> Tu	0016	11.4	347	
	0604	-1.0	-30		0631	0.6	18		0739	-1.3	-40		0716	0.4	12		0627	-1.8	-55	
	1219	11.5	351		1241	9.5	290		1354	10.8	329		1327	9.1	277		1242	11.2	341	
	1841	-1.9	-58		1857	0.1	3		2005	-1.3	-40		1932	0.4	12		1850	-1.5	-46	
<b>12</b> Su	0058	10.5	320	<b>27</b> M	0110	8.8	268	<b>12</b> W	0224	10.7	326	<b>27</b> Th	0145	9.2	280	<b>12</b> W	0106	11.2	341	
	0659	-1.0	-30		0707	0.7	21		0836	-0.9	-27		0755	0.4	12		0720	-1.6	-49	
	1313	11.2	341		1317	9.3	283		1451	10.1	308		1406	8.9	271		1335	10.6	323	
	1934	-1.7	-52		1931	0.2	6		2100	-0.7	-21		2011	0.6	18		1941	-1.0	-30	
<b>13</b> M	0152	10.4	317	<b>28</b> Tu	0145	8.8	268	<b>13</b> Th	0320	10.3	314	<b>28</b> F	0224	9.2	280	<b>13</b> Th	0157	10.8	329	
	0756	-0.8	-24		0745	0.8	24		0937	-0.5	-15		0838	0.5	15		0814	-1.1	-34	
	1410	10.8	329		1356	9.0	274		1552	9.4	287		1450	8.6	262		1430	10.0	305	
	2028	-1.3	-40		2007	0.4	12		2159	-0.1	-3		2054	0.8	24		2034	-0.3	-9	
<b>14</b> Tu	0248	10.3	314	<b>29</b> W	0222	8.8	268	<b>14</b> F	0420	9.9	302	<b>29</b> Sa	0251	10.3	314	<b>14</b> F	0251	10.3	314	
	0856	-0.5	-15		0826	0.9	27		1042	0.0	0		0911	-0.5	-15		0911	-0.5	-15	
	1510	10.2	311		1437	8.7	265		1657	8.9	271		1528	9.3	283		1528	9.3	283	
	2125	-0.8	-24		2046	0.7	21		2301	0.5	15		2130	0.3	9		2130	0.3	9	
<b>15</b> W	0348	10.1	308	<b>30</b> Th	0303	8.8	268	<b>15</b> Sa	0523	9.5	290	<b>30</b> Su	0348	9.8	299	<b>15</b> Sa	0348	9.8	299	
	1000	-0.2	-6		0912	1.0	30		1149	0.3	9		1012	0.1	3		1012	0.1	3	
	1614	9.6	293		1522	8.4	256		1804	8.5	259		1629	8.7	265		1629	8.7	265	
	2226	-0.3	-9		2130	0.9	27						2230	0.9	27		2230	0.9	27	
				<b>31</b> F	0348	8.8	268										<b>31</b> M	0333	9.6	293
					1002	1.0	30											0958	0.3	9
					1613	8.2	250											1615	8.6	262
					2218	1.0	30											2217	1.0	30

Time meridian 75° W. 0000 is midnight. 1200 is noon.  
 Heights are referred to mean lower low water which is the chart datum of soundings.

### Boston Harbor (Deer Island Light), Massachusetts, 1997

F—Flood, Dir. 254° True E—Ebb, Dir. 111° True

January				February				March															
Slack	Maximum																						
	h	m	knots																				
<b>1</b> W	0342	0824	1.0E	<b>16</b> Th	0421	0855	1.3E	<b>1</b> Sa	0442	0739	1.1E	<b>16</b> Su	0003	0331	1.0F	<b>1</b> Sa	0314	0600	1.2E	<b>16</b> Su	0424	0900	1.3E
<b>2</b> Th	1029	1233	1.0F	<b>17</b> F	1107	1430	1.0F	<b>2</b> Su	1136	1340	1.1F	<b>17</b> M	0554	1026	1.3E	<b>2</b> Su	1008	1211	1.2F	<b>17</b> M	1112	1436	1.0F
<b>3</b> F	1603	2045	0.9E	<b>18</b> Sa	1651	2123	1.2E	<b>3</b> M	1711	2003	1.0E	<b>18</b> Tu	1243	1605	1.0F	<b>3</b> M	1541	1821	1.0E	<b>18</b> Tu	1703	2130	1.1E
<b>4</b> Sa	2250	0100	1.1F	<b>19</b> Su	2330	0258	1.1F	<b>4</b> Tu	2354	0204	1.2F	<b>19</b> W	1834	2253	1.2E	<b>4</b> Tu	2226	0034	1.3F	<b>19</b> W	2334	0301	1.0F
<b>5</b> Su	0433	0914	1.0E	<b>20</b> M	0521	0953	1.3E	<b>5</b> W	0538	0848	1.1E	<b>20</b> Th	1342	1701	1.1F	<b>5</b> W	0406	0656	1.1E	<b>20</b> Th	0524	0959	1.3E
<b>6</b> M	1121	1329	1.0F	<b>21</b> Tu	1209	1532	1.0F	<b>6</b> Th	1809	2117	1.0E	<b>21</b> F	1941	2347	1.3E	<b>6</b> Th	1101	1304	1.2F	<b>21</b> F	1213	1536	1.0F
<b>7</b> Tu	1657	2136	0.9E	<b>22</b> W	1753	2221	1.2E	<b>7</b> F	2048	0201	1.1F	<b>22</b> W	2321	0129	1.2F	<b>7</b> F	1637	1921	1.0E	<b>22</b> W	1806	2227	1.2E
<b>8</b> W	2340	0155	1.1F	<b>23</b> Th	0030	0357	1.1F	<b>8</b> Sa	0049	0303	1.2F	<b>23</b> Th	0502	0801	1.1E	<b>8</b> Sa	2321	0129	1.2F	<b>23</b> Th	0036	0400	1.0F
<b>9</b> Th	0525	1003	1.1E	<b>24</b> F	0621	1050	1.4E	<b>9</b> Su	0634	1049	1.2E	<b>24</b> M	0502	0801	1.1E	<b>9</b> Su	0502	0801	1.1E	<b>24</b> M	0624	1054	1.3E
<b>10</b> F	1213	1431	1.1F	<b>25</b> Sa	1309	1630	1.1F	<b>10</b> M	1325	1545	1.2F	<b>25</b> Tu	1159	1402	1.2F	<b>10</b> M	1159	1402	1.2F	<b>25</b> Tu	1312	1633	1.0F
<b>11</b> Sa	1751	2225	1.0E	<b>26</b> Su	1856	2316	1.3E	<b>11</b> Tu	1907	2322	1.1E	<b>26</b> W	1737	2033	1.0E	<b>11</b> Tu	1737	2033	1.0E	<b>26</b> W	1911	2321	1.2E
<b>12</b> Su	0031	0254	1.2F	<b>27</b> M	0128	0453	1.1F	<b>12</b> W	0144	0407	1.3F	<b>27</b> Th	0019	0228	1.2F	<b>12</b> Su	0019	0228	1.2F	<b>27</b> Th	0133	0456	1.0F
<b>13</b> M	0618	1050	1.1E	<b>28</b> Tu	0720	1143	1.5E	<b>13</b> Th	0730	1145	1.3E	<b>28</b> F	0601	0923	1.2E	<b>13</b> M	0601	0923	1.2E	<b>28</b> F	0724	1147	1.4E
<b>14</b> Tu	1306	1605	1.1F	<b>29</b> W	1405	1724	1.1F	<b>14</b> F	1419	1717	1.3F	<b>29</b> M	1256	1507	1.2F	<b>14</b> Tu	1256	1507	1.2F	<b>29</b> M	1407	1726	1.1F
<b>15</b> W	1447	1749	1.3F	<b>30</b> Th	1958	0128	1.1F	<b>15</b> Sa	2004	0144	1.3F	<b>30</b> Su	1838	2300	1.1E	<b>15</b> W	1838	2300	1.1E	<b>30</b> Su	2023	0223	1.3E
<b>16</b> Th	2032	0031	1.2E	<b>31</b> F	0009	0009	1.4E	<b>16</b> Su	0014	0102	1.2E	<b>31</b> M	0118	0333	1.2F	<b>16</b> Th	0118	0333	1.2F	<b>31</b> M	0101	0101	1.3E
<b>17</b> F	2351	0106	1.3E	<b>1</b> Sa	0222	0546	1.2F	<b>17</b> M	0239	0522	1.4E	<b>1</b> Sa	0701	1123	1.3E	<b>17</b> M	0701	1123	1.3E	<b>1</b> Sa	0228	0547	1.1F
<b>18</b> Sa	0353	0636	1.5E	<b>2</b> Su	0815	1234	1.5E	<b>18</b> Tu	0825	1233	1.4F	<b>2</b> Su	1351	1652	1.2F	<b>2</b> Su	1351	1652	1.2F	<b>2</b> Su	0819	1236	1.4E
<b>19</b> Su	0942	1324	1.5E	<b>3</b> M	1457	1815	1.2F	<b>19</b> W	1510	1817	1.4F	<b>3</b> M	1938	2356	1.2E	<b>3</b> M	1938	2356	1.2E	<b>3</b> M	1455	1814	1.2F
<b>20</b> M	1624	1918	1.5F	<b>4</b> Tu	2054	0059	1.4E	<b>20</b> Th	2059	0102	1.3E	<b>4</b> Tu	2206	0211	1.4E	<b>4</b> Tu	2206	0211	1.4E	<b>4</b> Tu	2105	0105	1.4E
<b>21</b> Tu	2212	0106	1.3E	<b>5</b> W	0312	0635	1.2F	<b>21</b> F	0331	0629	1.5F	<b>5</b> W	0424	0745	1.2F	<b>5</b> W	0424	0745	1.2F	<b>5</b> W	0316	0635	1.1F
<b>22</b> W	2212	0106	1.3E	<b>6</b> Th	0906	1323	1.5E	<b>22</b> W	0919	1319	1.5E	<b>6</b> Th	1013	1432	1.4E	<b>6</b> Th	1013	1432	1.4E	<b>6</b> Th	0906	1323	1.4E
<b>23</b> Th	0353	0636	1.5E	<b>7</b> F	1544	1903	1.3F	<b>7</b> F	1601	1908	1.5F	<b>7</b> F	1647	2008	1.3F	<b>7</b> F	1647	2008	1.3F	<b>7</b> F	1539	1859	1.2F
<b>24</b> Th	0942	1324	1.5E	<b>8</b> Sa	2142	0147	1.4E	<b>8</b> Sa	2151	0148	1.4E	<b>8</b> Sa	2241	0255	1.3E	<b>8</b> Sa	2035	0217	1.4E	<b>8</b> Sa	2139	0146	1.4E
<b>25</b> F	1624	1918	1.5F	<b>9</b> Su	0400	0721	1.3F	<b>9</b> Su	0422	0723	1.3F	<b>9</b> Su	0505	0826	1.2F	<b>9</b> Su	0505	0826	1.2F	<b>9</b> Su	2129	0146	1.4E
<b>26</b> Sa	2212	0106	1.3E	<b>10</b> M	0951	1409	1.5E	<b>10</b> M	1011	1405	1.6E	<b>10</b> M	1050	1513	1.4E	<b>10</b> M	1050	1513	1.4E	<b>10</b> M	0947	1406	1.4E
<b>27</b> Su	0353	0636	1.5E	<b>11</b> Tu	1629	1948	1.3F	<b>11</b> Tu	1651	1957	1.6F	<b>11</b> Tu	1725	2047	1.3F	<b>11</b> Tu	1725	2047	1.3F	<b>11</b> Tu	1538	1852	1.5F
<b>28</b> Su	0942	1324	1.5E	<b>12</b> W	2223	0233	1.4E	<b>12</b> W	2242	0235	1.5E	<b>12</b> W	2315	0255	1.3E	<b>12</b> W	2315	0255	1.3E	<b>12</b> W	2219	0146	1.4E
<b>29</b> M	1624	1918	1.5F	<b>13</b> Th	0444	0806	1.3F	<b>13</b> Th	0513	0813	1.6F	<b>13</b> Th	0544	0903	1.2F	<b>13</b> Th	0544	0903	1.2F	<b>13</b> Th	0402	0714	1.5F
<b>30</b> M	2212	0106	1.3E	<b>14</b> Th	1033	1454	1.5E	<b>14</b> Th	1102	1451	1.6E	<b>14</b> Th	1127	1551	1.3E	<b>14</b> Th	0950	1355	1.6E	<b>14</b> Th	0402	0714	1.5F
<b>31</b> M	0353	0636	1.5E	<b>15</b> F	1710	2031	1.3F	<b>15</b> F	1740	2045	1.6F	<b>15</b> F	1802	2121	1.3F	<b>15</b> F	1628	1942	1.6F	<b>15</b> F	0402	0714	1.5F
	0942	1324	1.5E	<b>16</b> F	2302	0317	1.3E	<b>16</b> F	2332	0235	1.5E	<b>16</b> F	2350	0335	1.3E	<b>16</b> F	2221	0136	1.5E	<b>16</b> F	1628	1942	1.6F
	1624	1918	1.5F	<b>17</b> M	0527	0847	1.2F	<b>17</b> M	0532	0324	1.5E	<b>17</b> M	0623	0411	1.2E	<b>17</b> M	2221	0224	1.6E	<b>17</b> M	2221	0136	1.5E
	2212	0106	1.3E	<b>18</b> M	1112	1537	1.4E	<b>18</b> M	0605	0903	1.5F	<b>18</b> M	1203	1621	1.2E	<b>18</b> M	0453	0805	1.6F	<b>18</b> M	0453	0805	1.6F
	0353	0636	1.5E	<b>19</b> M	1750	2111	1.3F	<b>19</b> M	1830	2133	1.6F	<b>19</b> M	1840	2137	1.3F	<b>19</b> M	1042	1443	1.6E	<b>19</b> M	1042	1443	1.6E
	0942	1324	1.5E	<b>20</b> M	2340	0359	1.3E	<b>20</b> M	0022	0418	1.5E	<b>20</b> M	1919	2136	1.3F	<b>20</b> M	1718	2030	1.7F	<b>20</b> M	1718	2030	1.7F
	1624	1918	1.5F	<b>21</b> M	0608	0926	1.2F	<b>21</b> M	0022	0418	1.5E	<b>21</b> M	0026	0435	1.1E	<b>21</b> M	2311	0312	1.6E	<b>21</b> M	2311	0312	1.6E
	2212	0106	1.3E	<b>22</b> M	1151	1617	1.3E	<b>22</b> M	0022	0418	1.5E	<b>22</b> M	0026	0435	1.1E	<b>22</b> M	0545	0854	1.6F	<b>22</b> M	0545	0854	1.6F
	0353	0636	1.5E	<b>23</b> M	1830	2148	1.2F	<b>23</b> M	0022	0418	1.5E	<b>23</b> M	0026	0435	1.1E	<b>23</b> M	1133	1532	1.6E	<b>23</b> M	1133	1532	1.6E
	0942	1324	1.5E	<b>24</b> M	0017	0440	1.2E	<b>24</b> M	0022	0418	1.5E	<b>24</b> M	0026	0435	1.1E	<b>24</b> M	1807	2118	1.6F	<b>24</b> M	1807	2118	1.6F
	1624	1918	1.5F	<b>25</b> M	0649	0958	1.2F	<b>25</b> M	0022	0418	1.5E	<b>25</b> M	0026	0435	1.1E	<b>25</b> M	0545	0854	1.6F	<b>25</b> M	0545	0854	1.6F
	2212	0106	1.3E	<b>26</b> M	1229	1656	1.2E	<b>26</b> M	0022	0418	1.5E	<b>26</b> M	0026	0435	1.1E	<b>26</b> M	1133	1532	1.6E	<b>26</b> M	1133	1532	1.6E
	0353	0636	1.5E	<b>27</b> M	1910	2213	1.2F	<b>27</b> M	0022	0418	1.5E	<b>27</b> M	0026	0435	1.1E	<b>27</b> M	1807	2118	1.6F	<b>27</b> M	1807	211	

TABLE 2 - CURRENT DIFFERENCES AND OTHER CONSTANTS

No.	PLACE	Meter Depth	POSITION		TIME DIFFERENCES						SPEED RATIOS		AVERAGE SPEEDS AND DIRECTIONS							
			Latitude	Longitude	Min. before Flood		Flood		Min. Ebb		Ebb	h m	Dir.	knots	Dir.	knots	Dir.	knots	Dir.	
					h m	h m	h m	h m	Flood	Ebb										Minimum before Flood
BUZZARDS BAY <7>-cont. Time meridian, 75° W																				
2056	Penikese Island, 0.2 mile south of		41° 26.6'	West	-1 43	-0 15	-1 30	-2 39	0.4	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.9 287°	
2081	Gull and Nashawena I. between		41° 26.2'	70° 54.2'	-2 15	-0 57	-2 01	-2 41	0.5	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.1 247°	
2066	Weepocket Island, south of		41° 30.4'	70° 44.3'	-3 16	-1 07	-1 28	-2 27	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6 255°		
2071	Quaint Pissett Harbor entrance		41° 32.4'	70° 39.8'	Current weak and variable														0.4	
2076	West Palmouth Harbor entrance		41° 36.5'	70° 39.2'	Current weak and variable															0.3
2091	Magnasett Harbor		41° 38.9'	70° 39.2'	Current weak and variable															0.0
2086	Anelis Ledge, 0.4 mile south of		41° 41.1'	70° 35.4'	+0 26	-0 36	-0 06	-0 23	0.4	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0 216°	
2091	Dumpling Rocks, 0.2 mile southeast of		41° 32.0'	70° 57.1'	-1 43	-1 03	-1 32	-2 09	0.4	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.1 190°	
2096	Appogansett Bay		41° 35.1'	70° 57.1'	Current weak and variable															0.0
2101	Clarks Cove		41° 36'	70° 55'	Current weak and variable															0.0
2106	New Bedford Harbor and approaches		41° 35.6'	70° 50.4'	Current weak and variable															0.4
2111	West Island and Long Island, between		41° 34.0'	70° 46.6'	-0 43	-0 43	-1 28	-1 42	0.4	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.8 203°	
2116	West Island, 1 mile southeast of	6	41° 34.1'	70° 50.2'	Current weak and variable															0.3
2121	Nasketucket Bay		41° 37.1'	70° 47.1'	Current weak and variable															0.3
2126	Matapoisett Harbor		41° 38'	70° 41'	Current weak and variable															0.4
2131	Shippan Harbor		41° 41.4'	70° 44'	Current weak and variable															0.4
2136	Wareham River, off Long Beach Point		41° 44.0'	70° 43.0'	-1 41	-0 31	-1 22	-1 53	0.3	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6 203°	
2141	Wareham River, off Barney's Point		41° 44.7'	70° 42.4'	-1 49	-0 27	-1 22	-1 31	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6 185°	
on Cape Cod Canal, p.16																				
2146	Onset Bay, south of Onset Island		41° 43.9'	70° 38.7'	Current weak and variable															0.4
2151	Onset Bay, south of Wickes Island		41° 44.1'	70° 39.3'	Current weak and variable															0.8 203°
CAPE COD CANAL																				
2156	CAPE COD CANAL, railroad bridge		41° 44.5'	70° 36.8'	Daily predictions															4.5 250°
2161	Bourne Highway bridge		41° 45'	70° 35'	-0 03	-0 01	-0 03	-0 04	0.8	0.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	4.0 070°	
2166	Bourneade		41° 46'	70° 34'	-0 07	-0 03	-0 09	-0 10	0.8	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.3 065°	
2171	Sagamore Bridge		41° 46'	70° 33'	-0 09	-0 04	-0 11	-0 13	0.7	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	3.4 030°	
2176	Cape Cod Canal, east end	15	41° 46.5'	70° 30.0'	-0 13	-0 06	-0 17	-0 19	0.6	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.8 095°	
NARRAGANSETT BAY <8>																				
2181	Sakonnet River (except Narrows)				-3 26	-5 06	-2 48	-3 41	1.2	1.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.4 180°	
2186	Black Hill, SW of Sakonnet River	15	41° 30.4'	71° 13.2'	-2 54	-1 55	-2 13	-2 26	0.2	0.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4 012°	
2191	Almy Point Bridge, south of Sakonnet River	15	41° 37.3'	71° 13.2'	-3 00	-2 10	-2 30	-3 13	0.2	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.4 034°	
2196	Tiverton, Stone bridge, Sakonnet R. <9>		41° 37.5'	71° 13.0'	-2 58	-5 02	-2 26	-3 06	1.4	1.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.7 010°	
2201	Tiverton, RR. bridge, Sakonnet R. <10>		41° 38.3'	71° 12.9'	-3 26	-5 06	-2 48	-3 41	1.3	1.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6 010°	
2206	Common Fence Point, northeast of	10	41° 39.5'	71° 12.5'	-3 04	-1 15	-2 32	-2 41	1.2	1.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	2.3 000°	
2211	Brenton Point, 1.4 n. mi. southwest of	7	41° 25.9'	71° 22.6'	-1 03	-0 38	-1 20	-1 04	0.4	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.5 000°	
2216	Castle Hill, west of East Passage	15	41° 27.4'	71° 22.7'	-0 06	-0 42	-1 10	-0 29	0.4	0.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.1 046°	
2221	Bull Point, east of	10	41° 28.8'	71° 21.0'	-1 10	-0 47	-1 10	-1 33	0.6	0.8	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7 013°	
2226	Mackerel Cove		41° 29.5'	71° 22.8'	Current weak and variable															1.2 001°
2231	Newport Harbor, S and E. of Goat Island		41° 29'	71° 20'	Current weak and variable															0.6 170°
2236	Rose Island, northeast of	15	41° 30.2'	71° 19.9'	-1 57	-0 07	-1 17	-2 08	0.4	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.2 237°	
2241	Rose Island, northwest of	15	41° 30.4'	71° 21.1'	-1 38	-0 26	-1 38	-1 39	0.4	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0 190°	
2246	Rose Island, west of		41° 29.8'	71° 21.0'	-0 42	-0 30	-1 20	-1 28	0.4	0.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0 172°	
2251	Gould Island, southeast of	7	41° 31.5'	71° 20.2'	-1 42	-1 28	-1 14	-1 16	0.3	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.7 217°	
2256	Gould Island, west of	15	41° 31.9'	71° 21.5'	-0 16	-0 32	-1 13	-1 07	0.3	0.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.6 351°	

Endnotes can be found at the end of table 2.

# Pollock Rip Channel, Massachusetts, 1997

F—Flood, Dir. 035° True    E—Ebb, Dir. 225° True

January				February				March															
Slack	Maximum	Slack	Maximum	Slack	Maximum	Slack	Maximum	Slack	Maximum	Slack	Maximum	Slack	Maximum										
h m	h m	h m	h m	h m	h m	h m	h m	h m	h m	h m	h m	h m	h m										
1 W	0229 0819 1451 2033	0505 1135 1724 2356	1.7E 1.7F 1.6E 1.8F	16 Th	0259 0857 1530 2124	0543 1228 1814 2357	1.8E 2.0F 1.7E 1.7E	1 Sa	0326 0915 1600 2139	0603 1231 1831 2357	1.6E 1.7F 1.5E 1.5E	16 Su	0434 1037 1717 2313	0731 1419 2014 2313	1.8F 1.6E 2.0F 1.5E	1 Sa	0156 0741 1428 2008	0434 1053 1701 2317	1.7E 1.9F 1.6E 1.7F	16 Su	0303 0901 1545 2140	0550 1243 1834 2357	1.8F 1.6E 1.9F 1.5E
2 Th	0319 0910 1545 2126	0555 1229 1817 2356	1.6E 1.7F 1.5E 1.6E	17 F	0400 1001 1637 2231	0659 1338 1926 2357	2.0F 2.0F 1.6E 1.6E	2 Su	0420 1011 1658 2238	0654 1332 1929 2357	1.7F 1.8F 1.5E 1.5E	17 M	0535 1139 1818	0247 1520 2119	1.8F 2.1F 1.5E	2 Su	0248 0834 1525 2105	0525 1149 1757 2105	1.7E 1.8F 1.5E 1.5E	17 M	0405 1005 1648 2245	0659 1349 1944 2357	1.5E 1.9F 1.4E 1.4E
3 F	0409 1002 1640 2221	0650 1325 1912 2356	1.8F 1.6E 1.7F 1.5E	18 Sa	0501 1105 1741 2336	0208 0759 1444 2037	1.9F 1.7E 2.0F 1.5E	3 M	0515 1107 1755 2337	0155 0753 1433 2037	1.6F 1.8E 1.8F 1.5E	18 Tu	0614 1236 1913	0345 0938 1614 2214	1.9F 1.6E 2.2F 1.6E	3 M	0344 0932 1626 2208	0621 1253 1857 2208	1.8E 1.8F 1.5E 1.5E	18 Tu	0506 1107 1747 2345	0806 1449 2047 2357	1.7E 1.5E 2.0F 1.5E
4 Sa	0500 1054 1734 2315	0144 0739 1420 2007	1.8F 1.6E 1.8F 1.5E	19 Su	0601 1206 1842	0311 0903 1544	1.9F 1.7E 1.6E	4 Tu	0609 1203 1850	0256 0850 1532	1.7F 2.0F 1.6E	19 W	0724 1328 2001	0437 1028 1703	1.9F 1.7E 2.2F	4 Tu	0443 1034 1726 2311	0721 1401 1959 2311	1.6E 1.6E 1.5E 1.5E	19 W	0604 1204 1840	0906 1543 2142	1.6E 1.6E 1.6E
5 Su	0551 1145 1827	0238 0831 1512 2101	1.8F 1.7E 1.9F 1.6E	20 M	0637 1231 1937	0408 1001 1638	1.9F 1.7E 2.2F	5 W	0635 1257 1942	0353 0828 1532	1.8F 1.8E 1.9E	20 Th	0810 1410 2043	0523 1112 1746	2.0F 1.8E 2.3F	5 W	0543 1136 1825	0823 1507 2101	1.7E 2.0F 1.6E	20 Th	0638 1255 1928	0408 1632 2228	1.9F 1.6E 2.2F
6 M	0609 1234 1917	0330 0921 1601 2152	1.8F 1.8E 2.0F 1.7E	21 Tu	0747 1350 2026	0500 1051 1727	2.0F 1.8E 2.3F	6 Th	0753 1349 2032	0446 1037 1717	1.9F 2.0E 1.9E	21 F	0852 1450 2122	0604 1149 1824	2.0F 1.8E 2.3F	6 Th	0640 1235 1920	0923 1607 2200	1.8E 2.1F 1.8E	21 F	0742 1339 2010	1041 1715 2307	2.0F 1.7E 2.2F
7 Tu	0727 1322 2006	0418 1010 1648 2242	1.8F 1.9E 2.1F 1.8E	22 W	0833 1434 2110	0547 1134 1811	2.0F 1.8E 2.3F	7 F	0842 1439 2121	0536 1128 1805	2.1F 2.1E 2.4F	22 Sa	0931 1526 2159	0014 0641 1222	1.8E 2.0F 1.8E	7 F	0734 1330 2011	0431 1019 1700	2.0F 2.0F 1.9E	22 Sa	0208 0825 1420 2049	0535 1119 1753 2341	2.1F 1.8E 2.1F 1.8E
8 W	0814 1409 2053	0505 1058 1733 2330	1.9F 2.0E 2.3F 1.9E	23 Th	0912 1514 2150	0005 0629 1212 1850	1.7E 2.0F 1.8E 2.3F	8 Sa	0932 1529 2209	0001 0625 1218 1852	2.0E 2.2F 2.2E 2.5F	23 Su	1008 1600 2234	0045 0713 1253 1929	1.8E 2.0F 1.9E 2.2F	8 Sa	0202 0826 1423 2100	0523 1113 1750 2343	2.1F 2.1E 2.4F 2.1E	23 Su	0243 0904 1457 2126	0611 1153 1827 2357	2.1F 1.8E 2.2F 1.8E
9 Th	0901 1456 2140	0551 1145 1819	2.0F 2.1E 2.4F	24 F	0955 1551 2228	0041 0707 1246 1926	1.7E 1.9F 1.8E 2.2F	9 Su	1022 1619 2257	0050 0713 1308 1940	2.1E 2.3F 2.3E 2.5F	24 M	1046 1635 2310	0742 1326 1957	2.0F 1.9E 2.2F	9 Su	0918 1513 2148	1203 1838 255F	2.2E 2.5F 2.5F	24 M	0318 0941 1532 2201	0642 1225 1856 2357	2.1F 1.9E 2.2F 1.8E
10 F	0948 1544 2228	0637 1233 1906	2.1F 2.2E 2.5F	25 Sa	1034 1627 2305	0113 0741 1319 1958	1.7E 1.8F 1.9E 2.2F	10 M	1113 1709 2347	0139 0803 1358 2030	2.2E 2.3F 2.2E 2.5F	25 Tu	1124 1711 2347	0148 0811 1402 2027	1.9E 2.0F 1.9E 2.1F	10 M	0340 1006 1603 2236	0032 0659 1252 1925	2.2E 2.4F 2.5F 2.5F	25 Tu	0351 1018 1606 2237	0711 1258 1924 2357	2.1F 1.9E 2.1F 2.1F
11 Sa	1038 1633 2318	0725 1323 1954	2.1F 2.2E 2.5F	26 Su	1113 1703 2343	0146 0812 1354 2029	1.8E 1.9F 1.8E 2.1F	11 Tu	1206 1802 2347	0228 0855 1450 2123	2.1E 2.3F 2.2E 2.5F	26 W	1247 1749 2347	0224 0844 1441 2101	1.9E 2.0F 1.9E 2.1F	11 Tu	0428 1057 1653 2324	0748 1342 2013 2324	2.4F 2.2E 2.2E 2.4F	26 W	0424 1056 1642 2313	0740 1334 1954 2357	2.1F 1.9E 2.1F 1.8E
12 Su	1130 1725	0816 1414 2046	2.2F 2.2E 2.5F	27 M	1153 1740	0844 1431 2102	1.9F 1.8E 2.1F	12 W	1303 1857	0320 0951 1545 2221	2.1E 2.2F 2.0E 2.2F	27 Th	1247 1830	0303 0921 1524 2140	1.9E 2.0F 1.8E 2.0F	12 W	0517 1148 1743	0838 1432 2104	2.3F 2.1E 2.3F	27 Th	0459 1136 1720 2352	0812 1412 2028 2357	2.1F 1.9E 2.0F 1.8E
13 M	1224 1819	0248 0911 1508 2141	2.1E 2.1F 2.1E 2.4F	28 Tu	1235 1820	0258 0920 1512 2138	1.8E 1.9F 1.8E 2.0F	13 Th	1403 1956	0416 1054 1644 2325	1.9E 2.1F 1.8E 2.0F	28 F	1335 1916	0346 1004 1610 2225	1.8E 1.9F 1.7E 1.8F	13 Th	0014 0608 1243 1837	0257 0931 1525 2159	2.0E 2.2F 1.9E 2.1F	28 F	0537 1219 1802	0849 1455 2108	2.1F 1.9E 1.9F
14 Tu	1323 1917	0343 1011 1605 2242	2.0E 2.1F 2.0E 2.2F	29 W	1321 1904	0339 1000 1557 2219	1.8E 1.8F 1.7E 2.0F	14 F	1506 2100	0516 1202 1750 2100	1.8E 2.0F 1.6E 1.6E	14 F	1506 1934	0350 1030 1622 2300	1.9E 2.1F 1.8E 1.9F	14 F	0107 0702 1340 1934	0350 1030 1622 2300	1.9E 2.1F 1.8E 1.9F	29 Sa	0035 1306 1848	0314 0932 1542 2154	1.9E 2.0F 1.8E 1.8F
15 W	1425 2018	0441 1117 1707 2349	1.9E 2.0F 1.8E 2.1F	30 Th	1410 1951	0423 1045 1644 2306	1.8E 1.8F 1.7E 1.9F	15 Sa	1612 2207	0034 0621 1312 1902	1.9F 2.0E 1.6E 1.5E	15 Sa	1612 2207	0034 0621 1312 1902	1.9F 2.0E 1.6E 1.5E	15 Sa	0203 0759 1441 2035	0447 1135 1725 2035	1.7E 2.0F 1.6E 1.6E	30 Su	0122 0708 1359 1941	0402 1022 1633 2246	1.8E 2.0F 1.7E 1.7F
				31 F	1504 2043	1736 2357	1.6E 1.7F													31 M	0802 1457 2040	1119 1730 2348	1.9F 1.6E 1.6F

